

Precise Planning



# Preliminary Flood Study: 45 Noongah Street and 25 Gwynn Hughes Street, Bargo, NSW

ENVIRONMENTAL



WATER



WASTEWATER



GEOTECHNICAL



CIVIL



PROJECT  
MANAGEMENT



P1504816JR04V01  
July 2015

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**All enquiries regarding this project are to be directed to the Project Manager.**

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# **1 Introduction**

## **1.1 Overview**

Martens & Associates Pty Ltd has prepared this preliminary flood study to assess the flood extent and impact on the site known as 45 Noongah Street and 25 Gwynn Hughes Street, Bargo, NSW. This report has been prepared to support a proposed rezoning application for this site.

This report assesses the 1% Annual Exceedance Probability (AEP) and the Probable Maximum Flood (PMF) flood planning level.

## **1.2 Project Scope**

Project scope and objectives are:

1. Prepare a hydrologic model (DRAINS) for the site to determine the peak flows for the 1% AEP and the PMF storm events.
2. Prepare a hydraulic model (1D/2D SMS Tuflow) for the site under existing conditions for the 1% AEP and the PMF.
3. Prepare relevant flood maps including flood extents and levels.

## **1.3 Relevant Guidelines**

This report has been prepared in accordance with the following guidelines and policies:

- Institution of Engineers, Australia (2006) – *Australian Rainfall and Runoff*.
- Wollondilly Council (2008) – Stormwater Drainage Design “Design Specification D5”.
- Wollondilly Shire Council (2010) ‘Development Control Plan 2010’;
- Wollondilly Shire Council (2008) ‘Design Specifications: Sub-Division and Engineering Standards’.
- NSW Floodplain development manual (2005).

## 2 Hydrology Modelling

### 2.1 Overview

The DRAINS software package (version 2015.02 – 4 February 2015) was used with the RAFTS hydrological engine to assess the 1% AEP and the PMF peak flow rates for a range of storm durations between 5 mins and 4.5 hours.

### 2.2 Modelling Set-up

#### 2.2.1 Hydrological Model parameters

The RAFTS (storage routing) engine was used given the rural nature of the site and upslope sub-catchments. Parameters used in the model are based on figures given in Wollondilly Shire Council (2008) Engineering Design Specifications, and are shown in Table 1.

**Table 1:** Hydrologic modelling setup.

Parameter	Element	Value
IFD Data	2 year ARI 1 hour rainfall intensity <sup>1</sup>	32.0
	2 year ARI 12 hour rainfall intensity <sup>1</sup>	7.7
	2 year ARI 72 hour rainfall intensity <sup>1</sup>	2.2
	50 year ARI 1 hour rainfall intensity <sup>1</sup>	65.3
	50 year ARI 12 hour rainfall intensity <sup>1</sup>	15.3
	50 year ARI 72 hour rainfall intensity <sup>1</sup>	4.8
	G (skewness factor) <sup>2</sup>	0.02
Soil Properties	F2 <sup>2</sup>	4.29
	F50 <sup>2</sup>	15.75
	Impervious Area Initial Losses	0.0
	Impervious Area Continuous Losses	0.0
	Pervious Area Initial Losses	10.0
	Pervious Area Continuous Losses	2.5

**Notes:**

<sup>1</sup> - Figures for Bargo from Wollondilly Shire Council (2008) Engineering Design Specification D5 - Drainage Design.

<sup>2</sup> - Typical figures for Bargo given in Engineers Australia (2006).

#### 2.2.2 Sub-Catchment Properties

Sub-catchments used in the modelling were based on available topographic data provided by LPI and confirmed by site observations. Impervious area proportions were based on available aerial

photography. Sub-catchment boundaries used for modelling are provided in Attachment A. Catchment parameters are summarised below in Table 2.

**Table 2:** Details of catchments in RAFTS hydrological modelling.

Sub- Catchment	Area (ha)	Impervious (%)	Vectored Slope (%)	PERN Roughness
CAT 1	620.10	5	3	0.07
CAT 2	98.80	5	2.5	0.07
CAT 3	18.51	1	2.1	0.07
CAT 4	14.50	80	2.1	0.07
CAT 5	31.70	90	2	0.015
CAT 6A1 <sup>1</sup>	3.34	0	1.5	0.07
CAT 6A2 <sup>1</sup>	55.20	2.4	1.9	0.07
CAT 6A3 <sup>1</sup>	120.12	5.7	2.6	0.07
CAT 6B1 <sup>1</sup>	2.31	0	1.9	0.07
CAT 6B2 <sup>1</sup>	92.48	10.2	1.2	0.07
CAT 6B3 <sup>1</sup>	86.30	5	2.2	0.07
SITE	20.65	5	2.2	0.03

**Notes:**

<sup>1</sup> – Catchment details taken from previous modelling performed for 1A Kader Street, Bargo rezoning.

### 2.2.3 Results

DRAINS modelling results indicated that storm durations of 2 hours and 3 hours resulted in peak critical flows. Cat 1 produces its peak critical flow during the 3 hour storm, while the other catchments produce their peak critical flows during the 2 hour storm.

Results of peak flow rates for each catchment for the 1% AEP and PMF storms are summarised in Table 3.

**Table 3:** Details of catchments in RAFTS hydrological modelling.

Sub- Catchment	Storm Event	Duration (Hrs)	Peak Flow (m <sup>3</sup> /s)
CAT 1	1% AEP	2	55.51
CAT 2	1% AEP	2	12.26
CAT 3	1% AEP	2	2.52
CAT 4	1% AEP	2	6.39
CAT 5	1% AEP	2	18.01
OF 6 <sup>1</sup>	1% AEP	2	41.47
SITE	1% AEP	2	5.61
CAT 1	1% AEP	3	58.54
CAT 2	1% AEP	3	11.82
CAT 3	1% AEP	3	2.40
CAT 4	1% AEP	3	4.36
CAT 5	1% AEP	3	9.68
OF 6 <sup>1</sup>	1% AEP	3	40.66
SITE	1% AEP	3	4.54
CAT 1	PMF	2	334.60
CAT 2	PMF	2	60.76
CAT 3	PMF	2	11.89
CAT 4	PMF	2	11.55
CAT 5	PMF	2	25.64
OF 6 <sup>1</sup>	PMF	2	215.01
SITE	PMF	2	15.25
CAT 1	PMF	3	310.74
CAT 2	PMF	3	54.97
CAT 3	PMF	3	10.58
CAT 4	PMF	3	9.66
CAT 5	PMF	3	22.12
OF 6 <sup>1</sup>	PMF	3	193.81
SITE	PMF	3	12.55

**Notes:**

<sup>1</sup> - OF6 refers to the cumulative flow generated by sub-catchments 6A1, 6A2, 6A3, 6B1, 6B2 and 6B3.



## 3 Hydraulic Modelling

### 3.1 Overview

The SMS Tuflow 1D/2D hydraulic model (SMS 11.2.9 13 Mar 2015) was used to determine existing condition flood water levels and extents for the 1% AEP and PMF storm events.

### 3.2 Topographic Data

2m topographic data provided by LPI was used to create a 3D surface for the site and the local floodplain environment used in the Tuflow model.

### 3.3 Modelling Set-up

Tuflow model construction consisted of:

1. Development of a 2.0m x 2.0m topographic grid for the 1% AEP storm event simulation, and a 4.0m x 4.0m topographic grid for the PMF storm event simulation.
2. Position inflow boundary conditions based on the 1% AEP critical storm duration and the PMF DRAINS model hydrographs.
3. Establishment of model boundary extents.
4. A 2% computed water slope for the downstream model boundary extent was defined, based on the floodplain slopes of the available topographic data.
5. Assigning manning's roughness coefficients based on SIX Maps Viewer Aerials (2014) for hydraulic modelling as shown in Table 4.
6. Incorporation of blockages to simulate existing buildings.

**Table 4:** Mannings roughness coefficients used in SMS Tuflow modelling.

Catchment Material	Manning's Roughness Applied
Building	0.2
Forest Riparian	0.07
Grassed	0.035
Road	0.012
Urban	0.1

### **3.4 Results**

Results of flood levels and extents for the 1% AEP and PMF critical storm events for existing conditions are given in Attachment C.

## 4 References

Institution of Engineers, Australia (2006) – *Australian Rainfall and Runoff*

Land and Property Information NSW (2014) – *SIX Maps Viewer*

NSW Floodplain development manual (2005).

O'Loughlin, G., Stack, B., (2014) - *DRAINS User Manual*

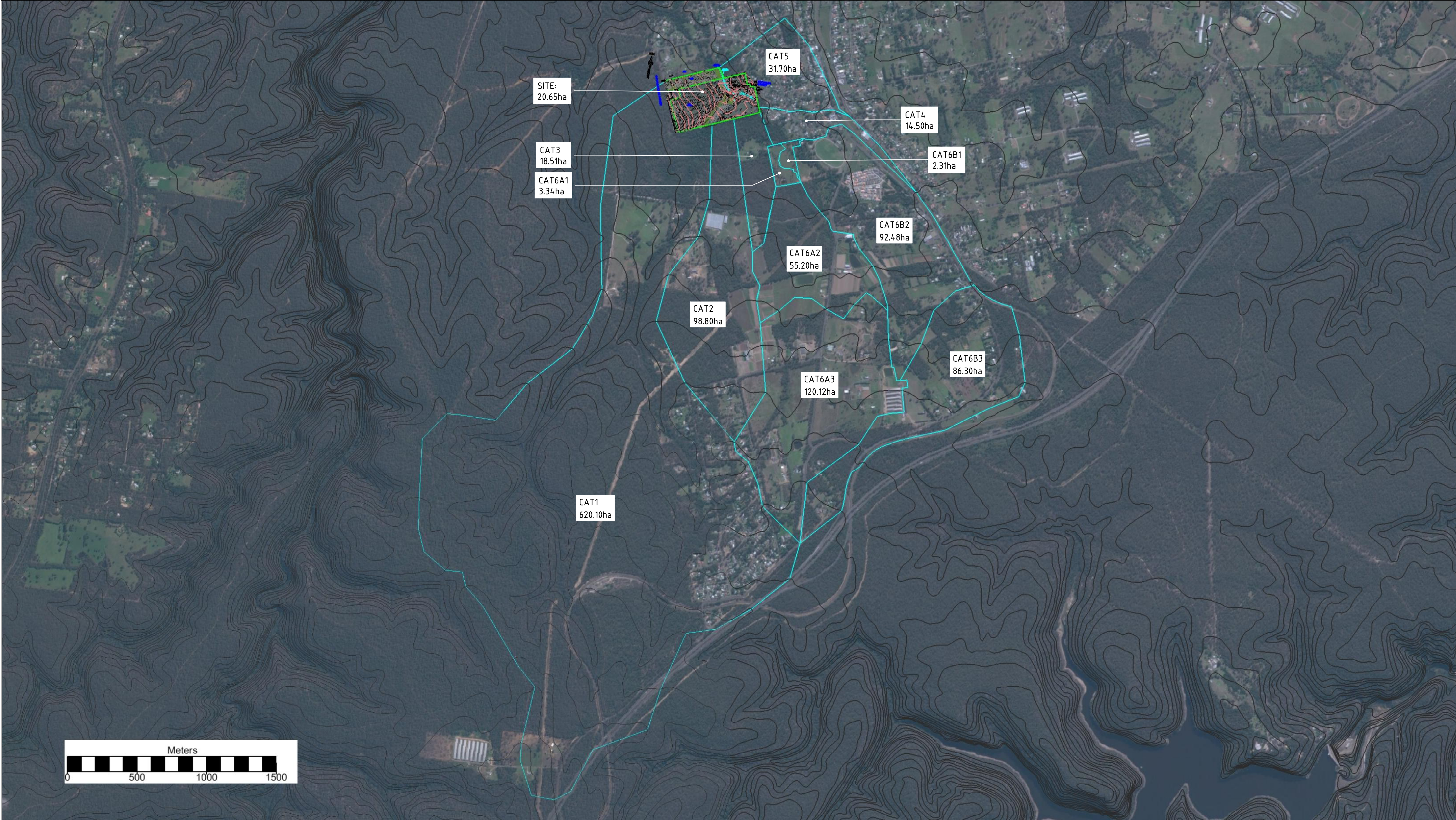
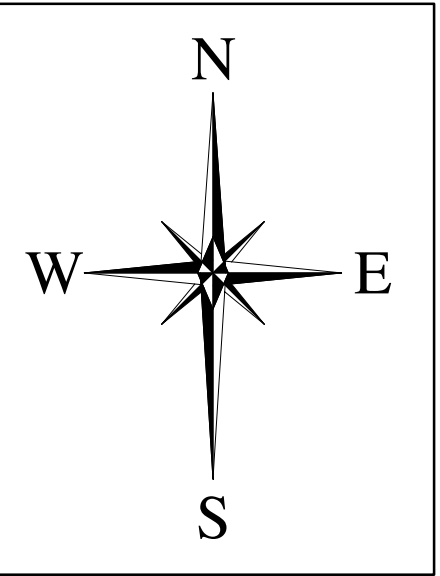
Wollondilly Council (2008) – *Stormwater Drainage Design "Design Specification D5"*.

Wollondilly Shire Council (2010) '*Development Control Plan 2010*';

Wollondilly Shire Council (2008) '*Design Specifications: Sub-Division and Engineering Standards*'.

## 5      **Attachment A: Catchment Plan & Existing Site Survey**





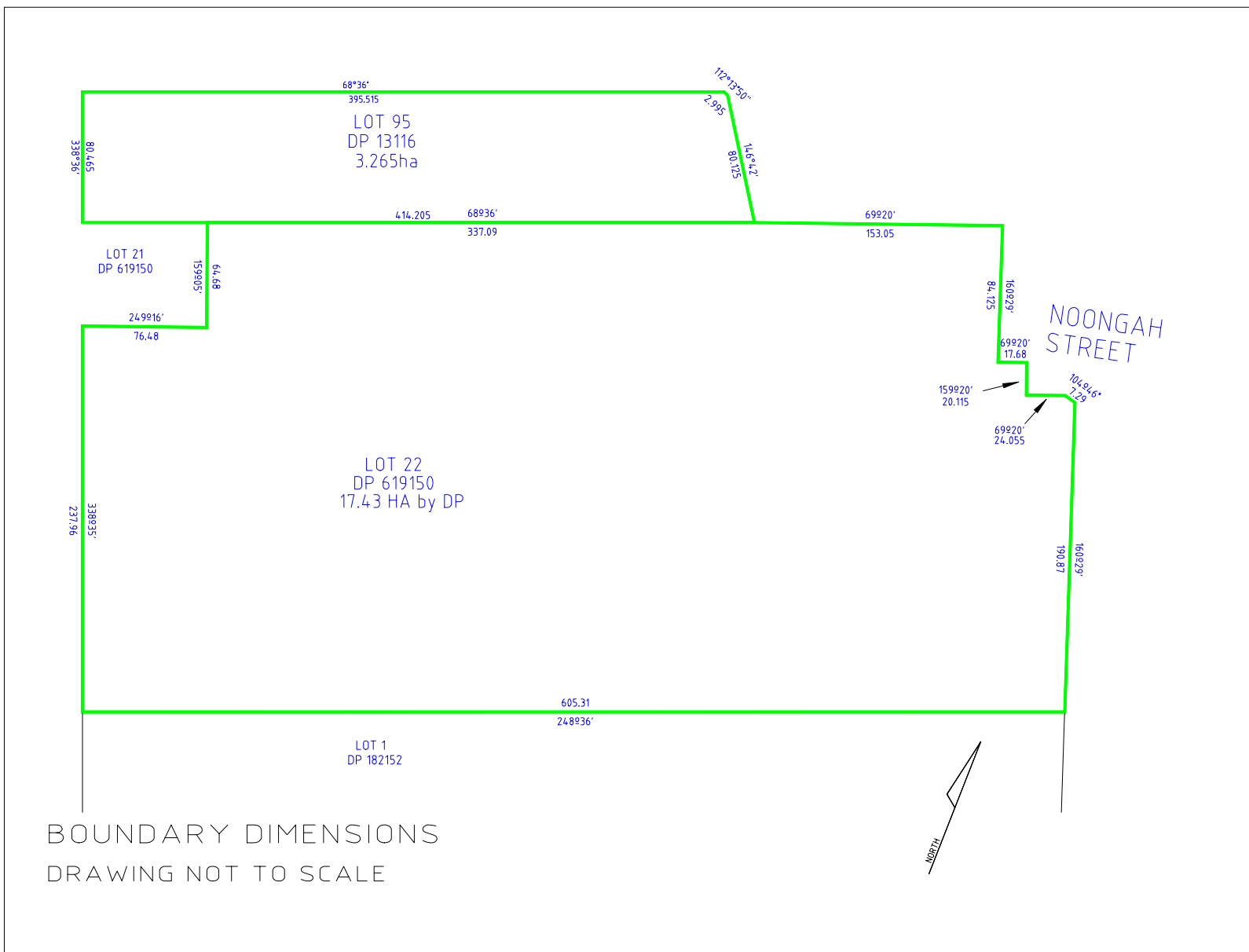
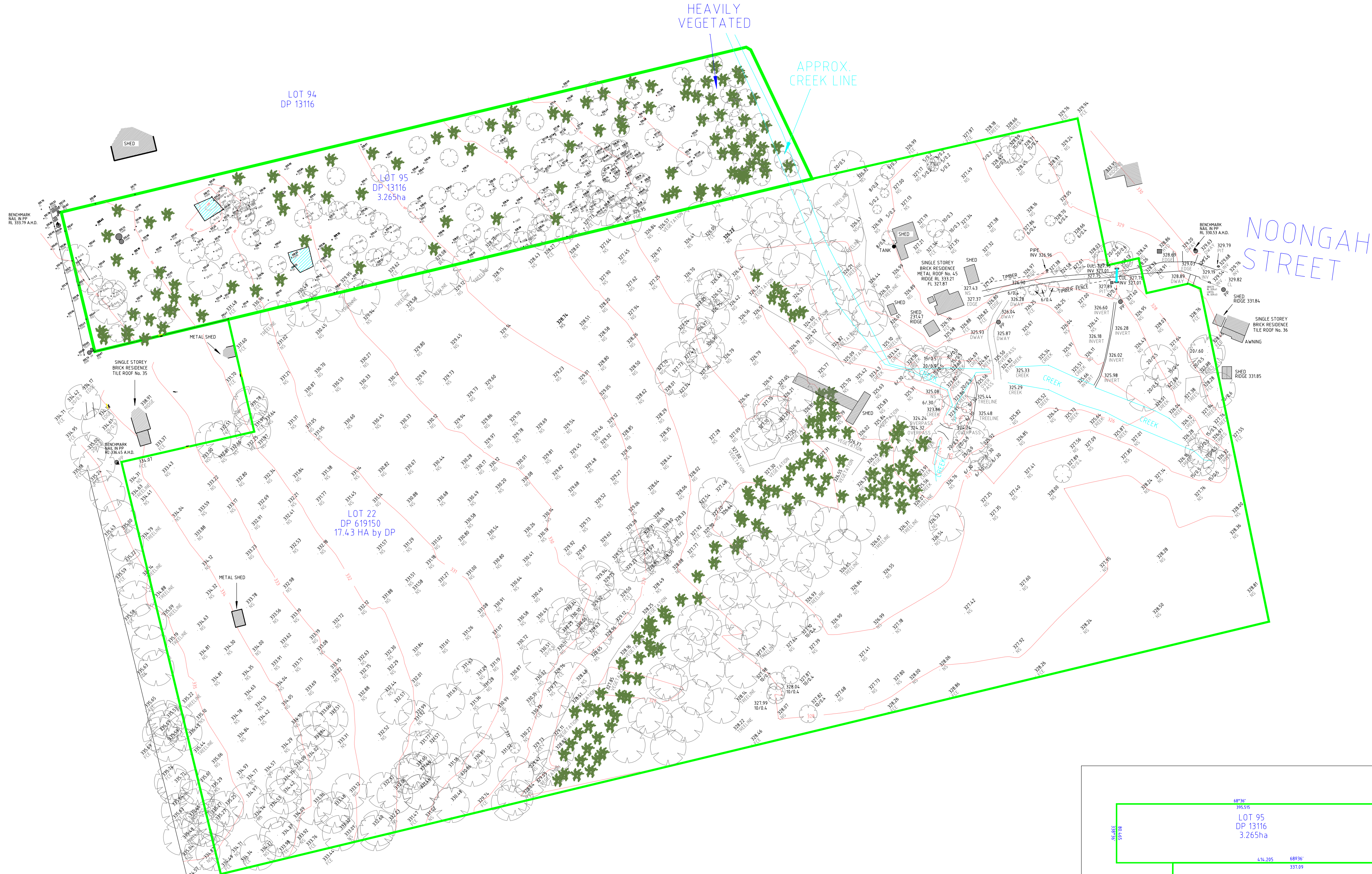
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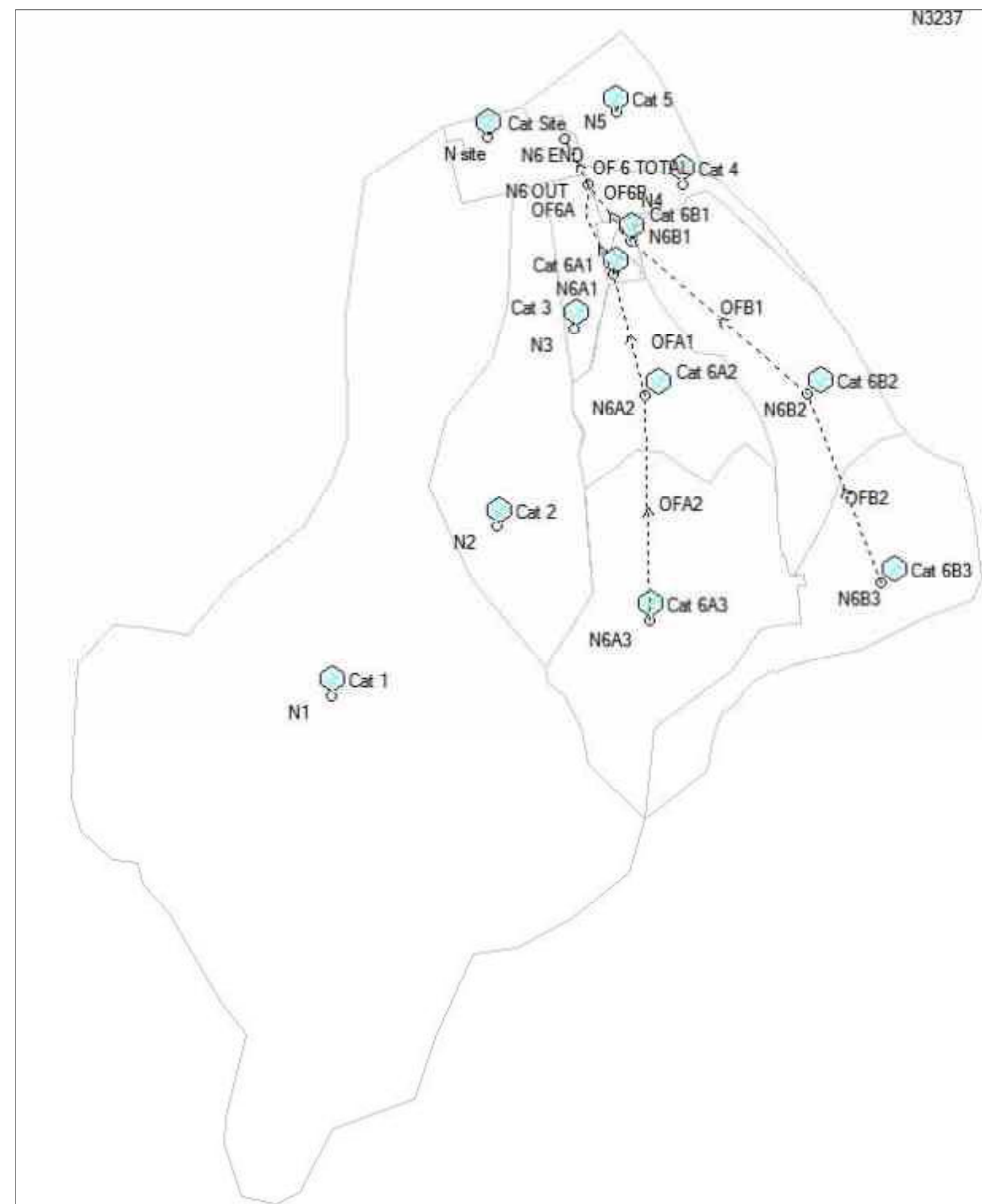


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## 6      **Attachment B: DRAINS Model layout and results**



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A map of the study area, which is an irregularly shaped land parcel. The map shows several sampling points marked with blue hexagons and labeled with numerical values. The values are: 4.54, 9.68, 4.36, 0.365, 20.2, 20.8, 0.491, 2.4, 20.4, 6.01, 9.92, 11.8, 14.4, 14.4, 10.1, and 58.5. Distances between points are indicated by red dashed lines with arrows, labeled with values: 40.7, 20.2, 20.8, 20, 20.4, 14.4, 10.1, and 14.4. The map also shows a network of roads and a river or canal system.

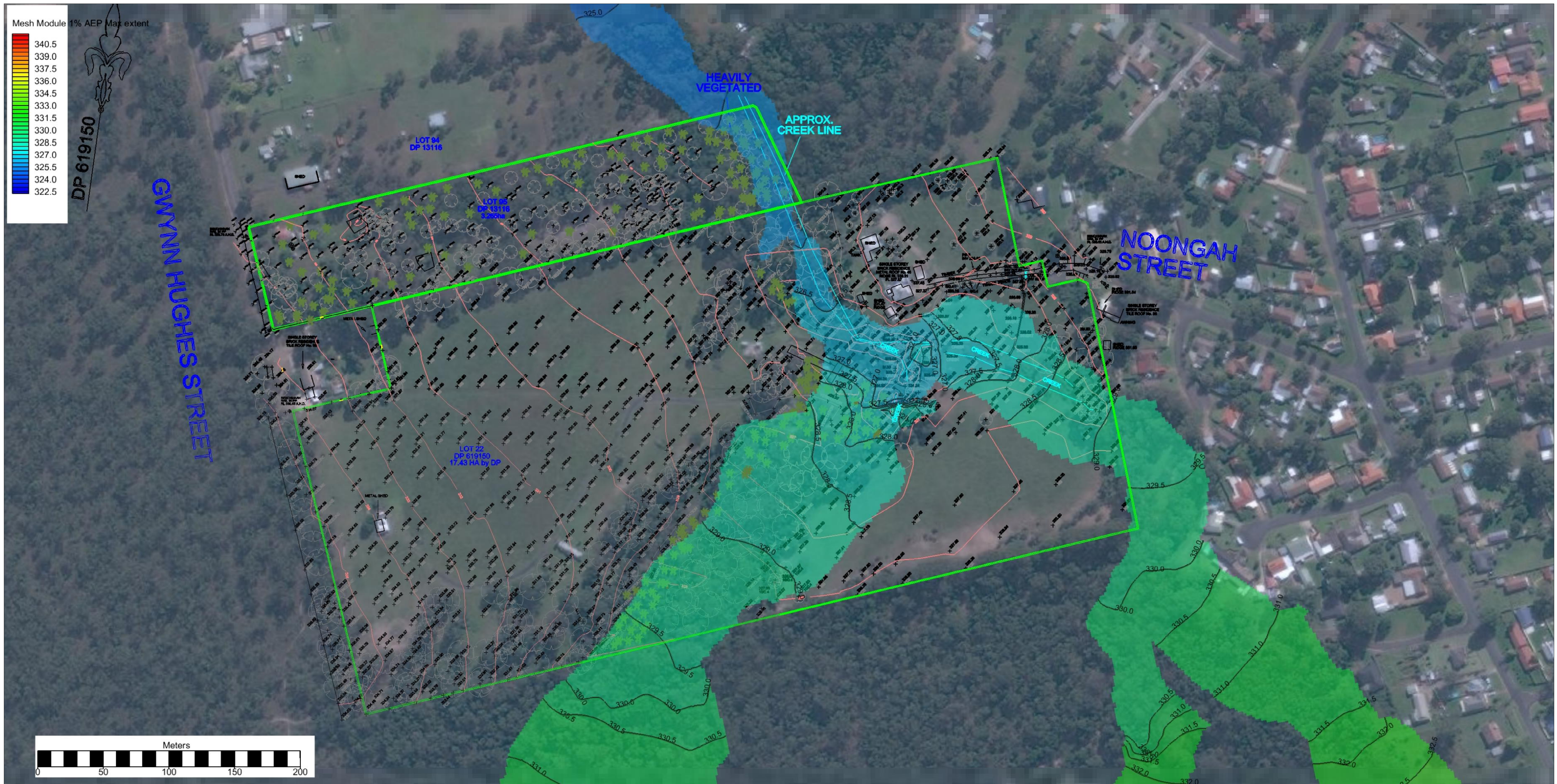
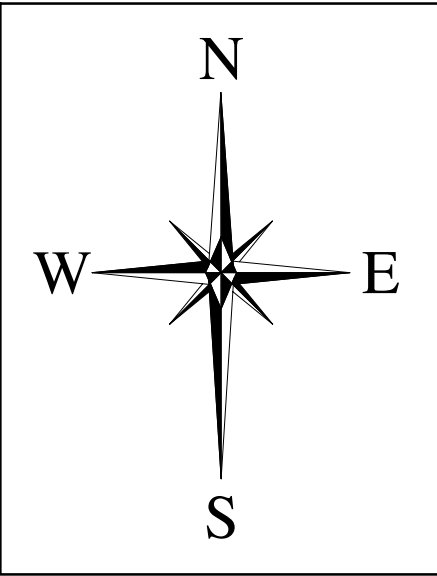
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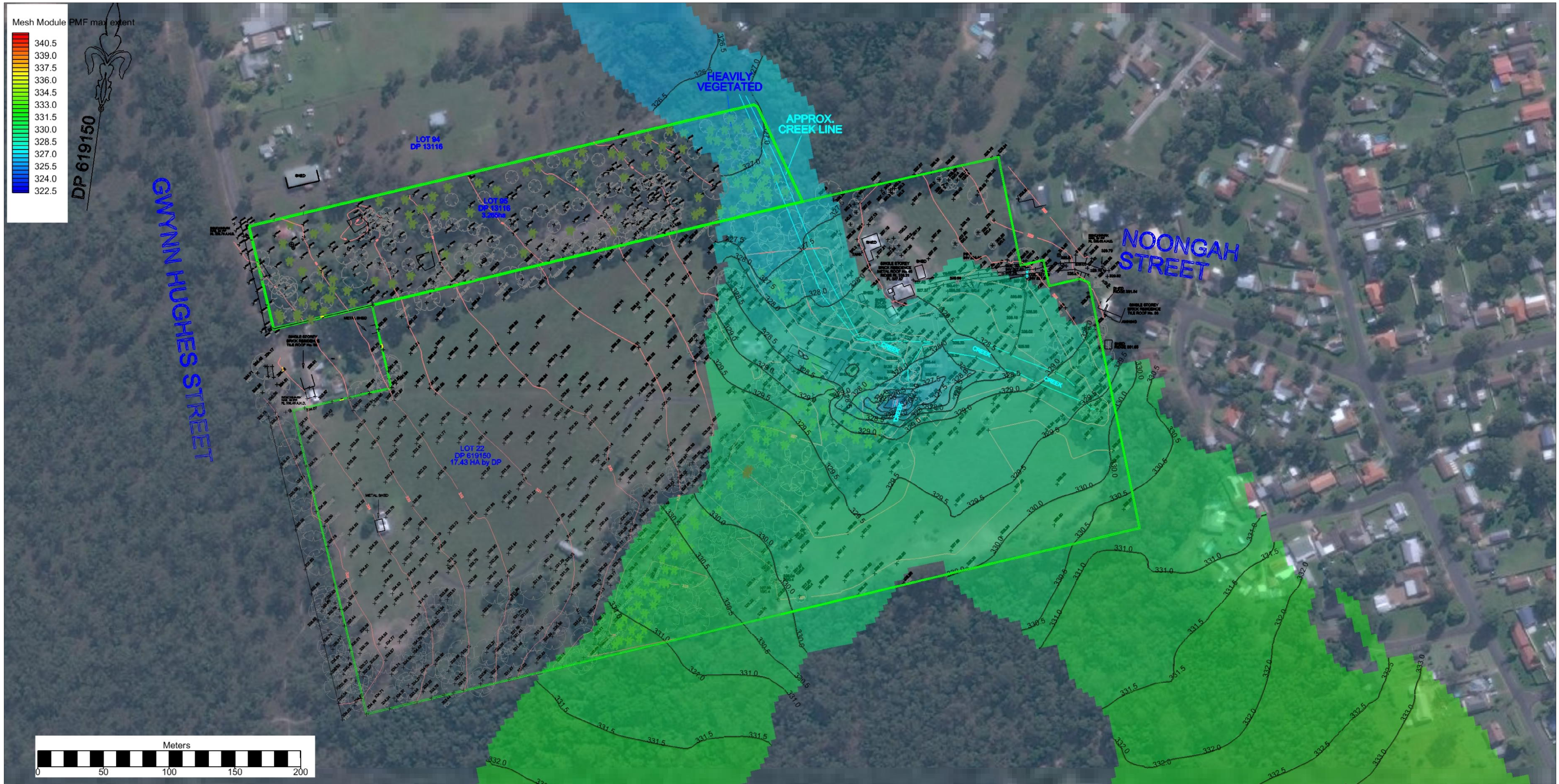
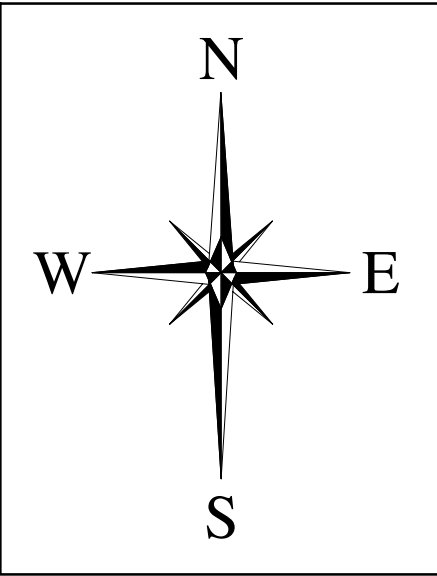
## 7      **Attachment C: Flood Images**





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